## 6.3.2 Horizontal Disperse Flow

As might be expected, frictional losses in straight uniform pipe flows have been the most widely studied and so it is appropriate to begin with a discussion of that subject, focusing first on disperse or nearly disperse flows and then on separated flows.

Beginning with disperse horizontal flow, it is noted that there exists a substantial body of data relating to the frictional losses or pressure gradient, (-dp/ds), in a straight pipe of circular cross-section (the coordinate s is measured along the axis of the pipe). Clearly (-dp/ds) is a critical factor in the design of many systems (for example slurry pipelines). This pressure gradient is usually non-dimensionalized using the pipe diameter, d, the density of the continuous phase  $(\rho_C)$ , and either the total volumetric flux, j, or the volumetric flux of the continuous fluid  $(j_C)$ . Thus, commonly used friction coefficients are

$$C_f = \frac{d}{2\rho_C j_C^2} \left( -\frac{dp}{ds} \right) \quad \text{or} \quad C_f = \frac{d}{2\rho_C j^2} \left( -\frac{dp}{ds} \right) \tag{1}$$

and, in parallel with the traditional Moody diagram for single phase flow, these friction coefficients are usually presented as functions of a Reynolds number for various mixture ratios as characterized by the volume fraction,  $\alpha$ , or the volume quality,  $\beta$ , of the disperse phase. Commonly used Reynolds numbers are based on the pipe diameter, the viscosity of the continuous phase ( $\nu_C$ ) and either the total volumetric flux, j, or the volumetric flux of the continuous phase,  $j_C$ . For boiling flows or for gas/liquid flows, the reader is referred to the reviews of Hsu and Graham (1976) and Collier and Thome (1994). For a review of slurry pipeline data the reader is referred to Shook and Roco (1991) and Lazarus and Neilsen (1978). For the solids/gas flows associated with the pneumatic conveying of solids, Soo (1983) provides a good summary.